

Introduction

If a chain is only as strong as its weakest link, a pipeline is only as strong as its weakest weld. It's therefore not surprising that a huge amount of energy is expended on the process of welding pipes to tight specifications. This in turn can lead to bottle necks in the welding process if the specification cannot be easily met. OMS have worked with the industry owners, pipelay contractors and welders in order to develop solutions to these problems.

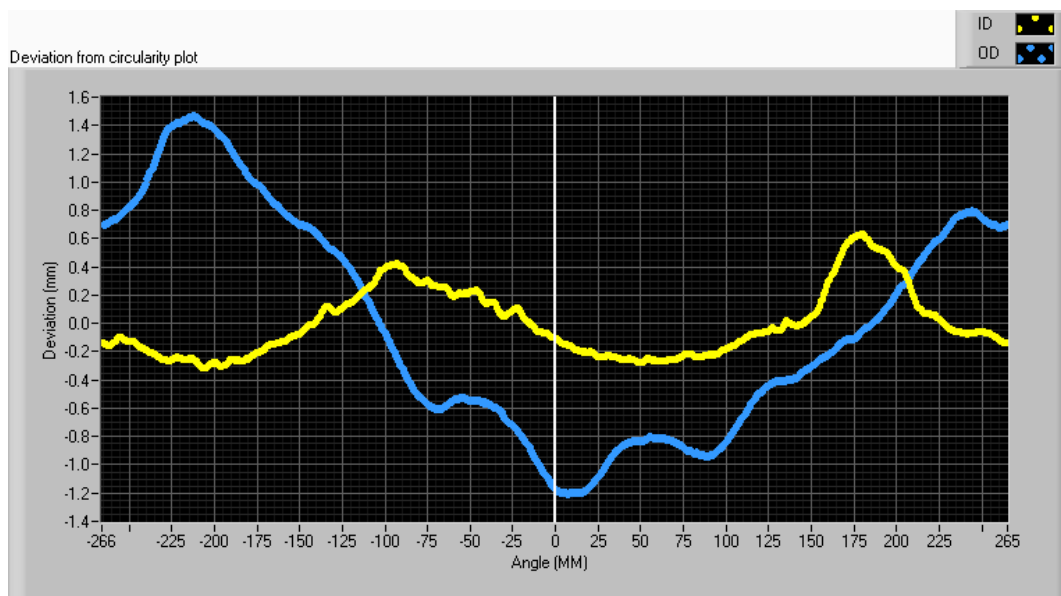
If pipes were round and of the same size there would be no fit up problems. Unfortunately pipes are manufactured by processes which are not perfect. The result is variations in size and shape. The knock on effect is problems in pipe fit up and hence problems with welding and fatigue life.

This problem has a solution, to be exact, a variety of solutions depending on the type of pipe and the clients requirements. These solutions have all been tried and tested on projects around the world from Africa and Brazil to the Gulf of Mexico. Four examples are now given:

Example 1. Avoiding counterboring SCR pipes

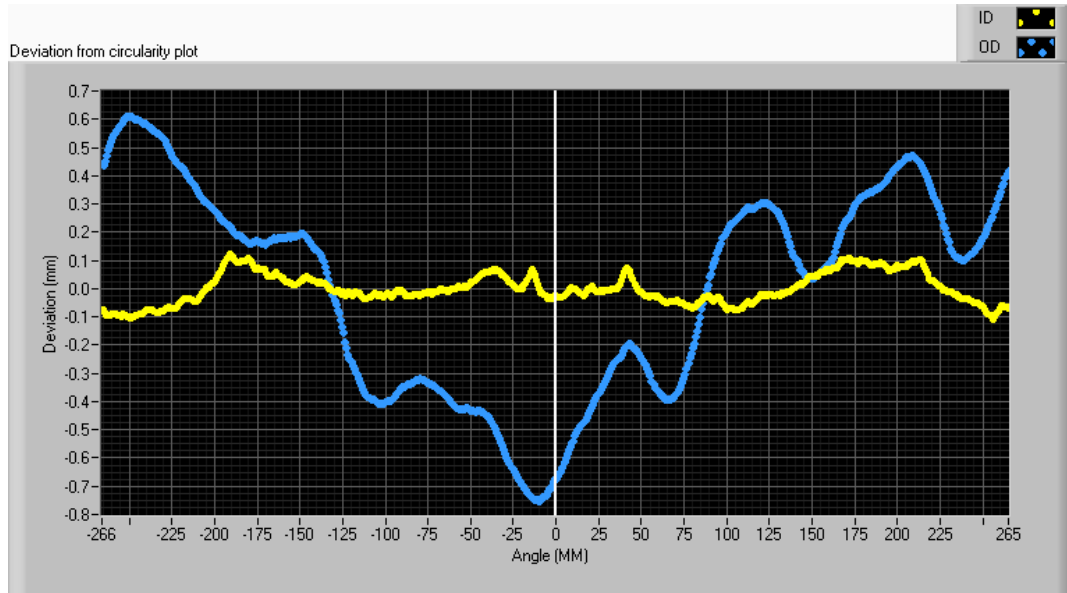
'A pipe that is round with a constant wall thickness does not exist'. In looking at thousands of pipes of many different sizes and from many pipe mills, we have not seen one anyway. Out of round pipes will give welding engineers problems. There may be insufficient wall thickness to counterbore or the design engineers may wish to retain as much wall thickness as possible. If pipes cannot be counterbored, how can these pipes meet an exacting internal fit up specification when randomly bringing the pipes together would not achieve the required fit-up criteria (generally 0.5mm or less HiLo)?

Some example pipe shapes are illustrated in the following graphs which are of pipes with average, maximum and minimum variations in the internal diameter from a set of pipes.

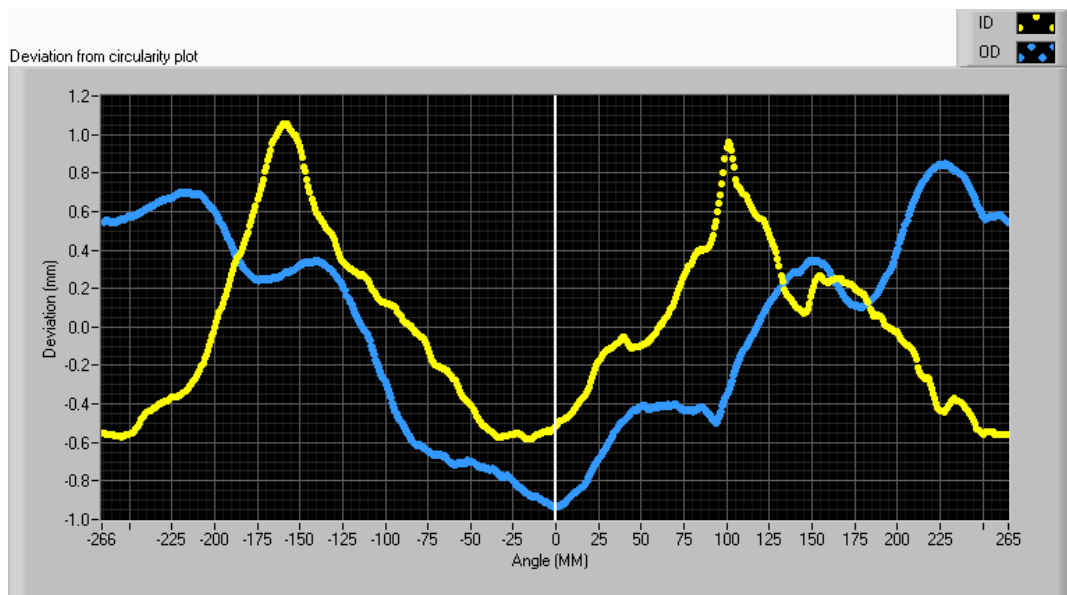


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Average variation in ID (Yellow line) is illustrated in this graph by the yellow line. The blue line represents the relative difference in Wall Thickness. If two pipes of the same shape and size as this pipe were matched the result could be a HiLo of more than 0.85 mm.



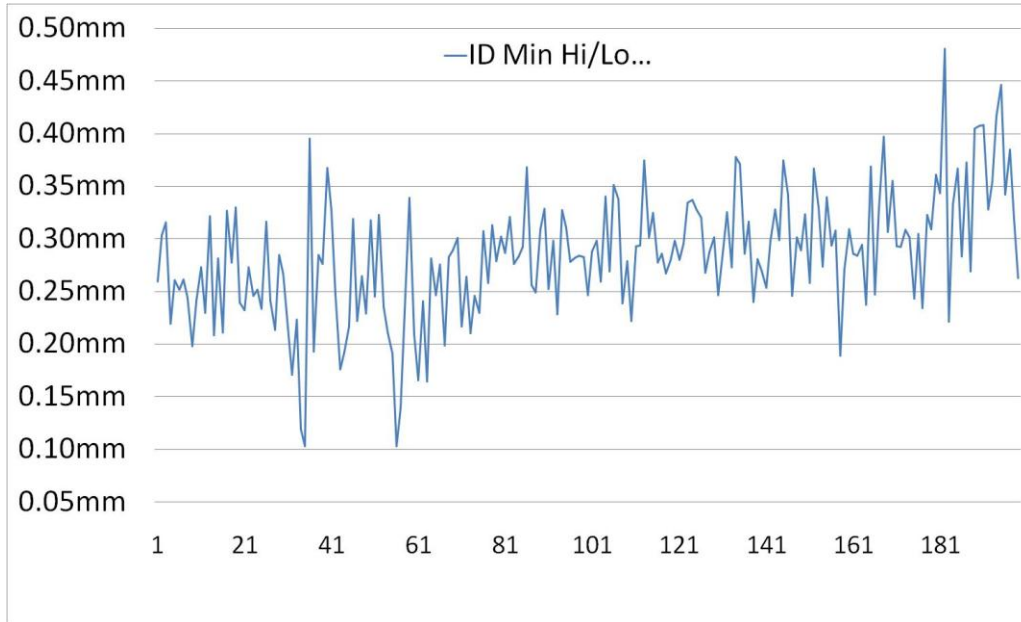
This graph illustrates the roundest pipe and the following graph illustrates the least round pipe.



This graph illustrates the least round graph with a variation in ID shape in excess of 1.6 mm.

The OMS solution to the problem presented by these pipes is to match the pipes together which are of the same size and shape. We have successfully managed a large number of projects, fitting together pipe which has not been counterbored, and have achieved fit-ups that have averaged better than 0.3 mm. Pipes can be used which have been cold end sized or directly without cold end sizing.

A typical HiLo maximum value graph is illustrated in the following figure.



In this case a HiLo average of around 0.3 mm was achieved. HiLo fit up average results between 0.25 mm and 0.35 mm are typical. A fit up of this level means that the pipes can be welded together with confidence that fit up will not be an issue for these pipes.

E.G. ATP Mirage, Callon - Entrada, BP - Greater Plutonio

Example 2. Avoiding wall thickness problems in SCR and Flowline pipe

Seamless pipes, by their nature, have very variable wall thicknesses. AUT (Automatic Ultrasonic Testing) requirements mean that the variability in the wall thickness in pipes can cause significant cost issues (i.e. if you are unable to construct a flowline or SCR with the minimum number of AUT scans). Furthermore, if the thick and thin parts of two pipes are brought together (pipes are usually lined up internally) then the outside of the two pipes will not match leaving an unacceptable HiLo difference (outside of the oil companies specification).

How has OMS solved this problem for its clients? There are a number of solutions. In one recent project in the US, the pipes were measured and sorted according to the required calibration blocks to be used for the AUT inspection. This sorting enabled the pipes that fell within a designated wall thickness range to be allocated to the more critical areas of the pipeline and the pipes that were more difficult to be fitted together were used in the less critical areas. A typical fragment of a SCR string with AUT cal block designations is shown in the following table.

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03150_B 03042_A	Aut Cal Block Group B	03408_A 03121_A	Aut Cal Block Group A	Critical
03042_B 03074_A		03121_B 03489_B		
03074_B 03424_B		03489_A 03507_A		
03424_A 03533_A		03507_B 03144_B		
03533_B 03561_B		03144_A 03174_A		
03561_A 03260_B		03174_B 03448_B		
03260_A 03364_B		03448_A 03618_B		
03364_A 03152_A		03618_A 03660_B		
03152_B 03545_A		03660_A 03655_A		
03545_B 03485_A		03655_B 03635_B		
03485_B 03089_A		03635_A 03546_A		
03089_B 03060_B		03546_B 03634_A		
03060_A 03172_B		03634_B 03624_B		
03172_A 03292_B		03624_A 03453_A		
03292_A 03509_B		03453_B 03263_A		
03509_A 03471_A		03263_B 03049_B		
03471_B 03433_A		03049_A 03212_B		
03433_B 03427_B		03212_A 03276_A		
03427_A 03432_B		03276_B 03019_B		
03432_A 03516_A		03019_A 03233_A		
03516_B 03096_A		03233_B 03428_A		
03096_B 03443_A		03428_B 03543_A		
03443_B 03134_B		03543_B 03295_A		
03134_A 03149_B		03295_B 03499_A		
03149_A 03452_A		03499_B 03488_B		
03452_B 04326_B		03488_A 03204_B		
04326_A 03456_B		03204_A 03258_A		
03456_A 03411_A		03258_B 03457_A		
03411_B 03408_B		03457_B 03380_A		

This identification meant that there was the least possible disruption to the fit-up process.

Another example involved assessing pipe dimensions in real time and marking pipes accordingly so that problem pipes were welded onshore and not offshore where they could have delayed production.



This example is illustrated in the figure above where a colour code end marking has been put onto the pipes. In this case the dual markings are because the pipe was measured at both 20 mm and 100 mm into the pipe and indicate that these pipes can be segregated into a pile where these pipes can be used both offshore and onshore.

Yet another example utilised the OMS visualisation software in the firing line to simultaneously optimise both the ID and OD fit-up between the pipes.

E.G. Petrobras - Cascade Chinook, BP Thunderhorse, Shell BC 10.

Example 3. Avoiding bad fit up delays on board “J-lay” vessels

When a quad, quin or hex is raised in the tower and butted onto the previous set of pipes (that has been lowered into the water) the weld must be completed as quickly as possible to maintain the pipelay schedule. When a pipe does not make the HiLo requirement it may have to be lowered back to the deck and a replacement pipe used. Alternatively the pipe may have been welded and then the hi/lo is measured and then a cut out may result due to the excessive HiLo.

The OMS solution is to measure the pipes onshore and then give the client software which enables them to visualise the fit up before they put the pipes into the firing line. A rotation of the pipe can be performed to gain the best fit possible or, if a fit-up is not possible at all, the pipe can be put to one side

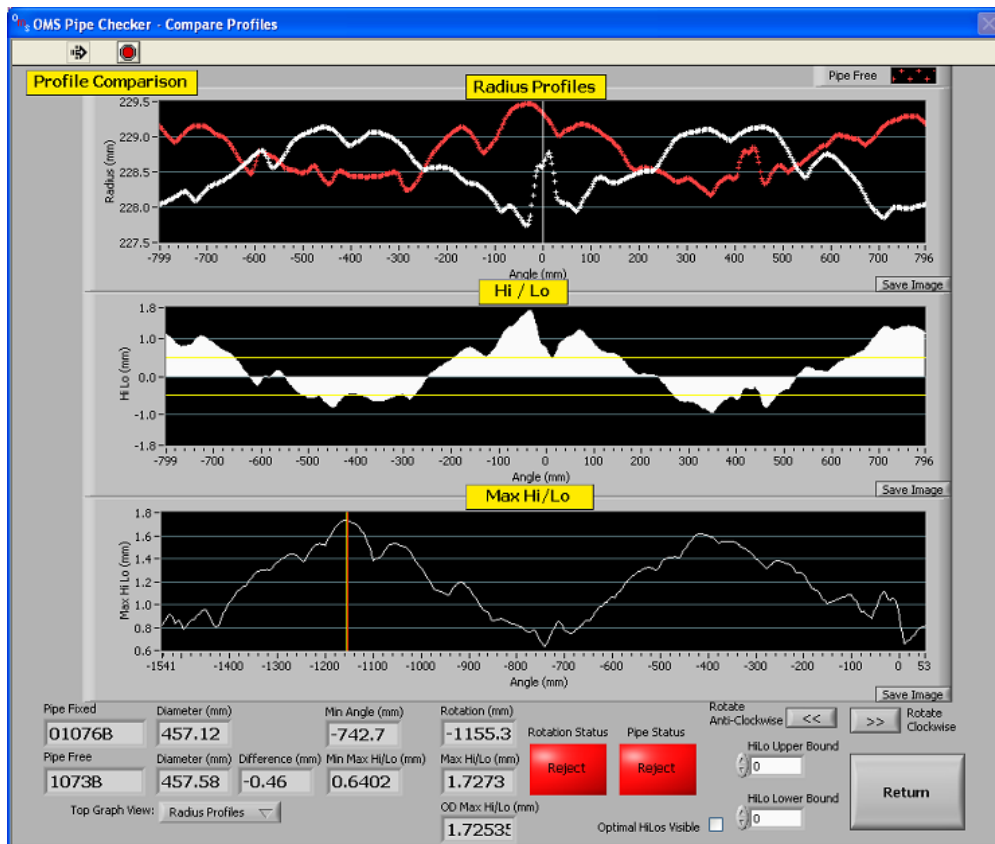
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and a better candidate selected. Our clients report that this methodology has completely solved all welding and fit-up problems for them on board the pipe lay vessels.

The system works by knowing what the fit up problems are likely to be before you have them and then offers a solution to deal with them. In our experience most fit ups can be dramatically improved by early identification of shape and by rotating the pipes in respect to each other. OMS software identifies the rotation required and the pipe just needs to be rotated to the correct rotation before welding. This scheme works well for oval pipes as you just match the two ovals together to solve the problem. It also works for other misshapen pipes. In the few cases that this solution will not work – for example when you are trying to match a round pipe and an oval pipe or when the pipes are both different in size and shape - the pipe is held back until it can be fitted up to a similar pipe. It is only pipes which are damaged or have a serious manufacturing defects that cannot be used at all.

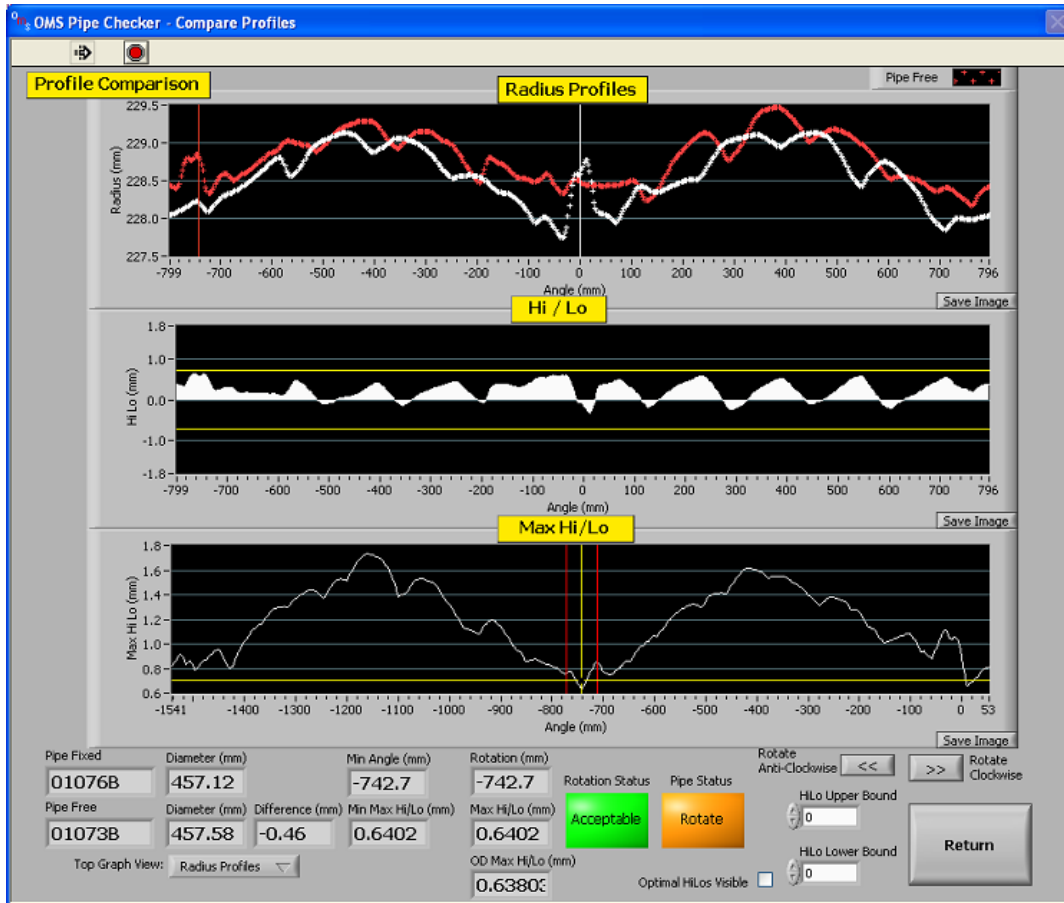
How can you never introduce a fit up problem to the firing line? The following two graphs explain the process:

The first figure illustrates the worst case fit up of two 18” pipes.



The top graph is the radial distance from the centre of the pipes – both of them are oval. The middle graph is the HiLo fit up plot showing that mismatch between the pipes would be more than 1.7 mm.

The next graph show what happens when you rotate the two pipes into the best rotation position.



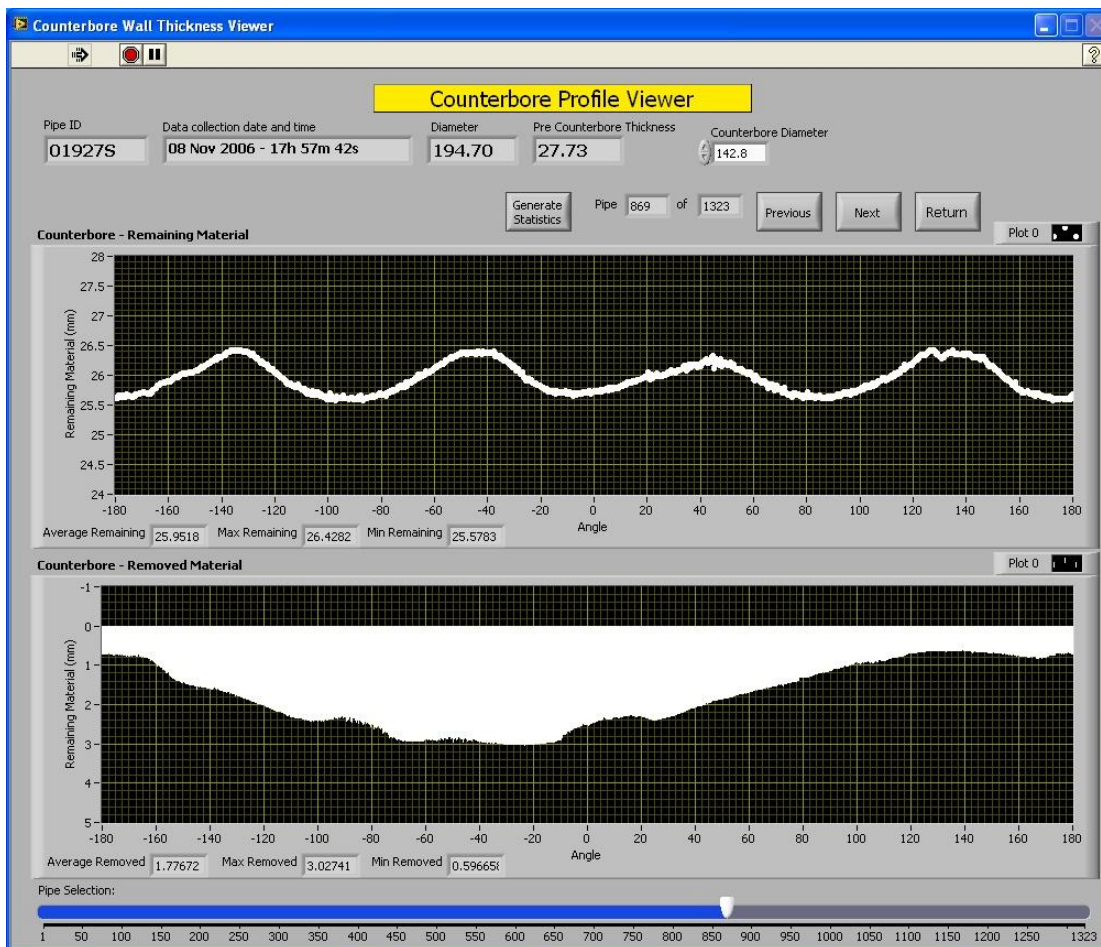
Here you can see that the two pipes are now meshed together and the maxim HiLo anywhere around the pipe could be as small as 0.7 mm. Much of the HiLo is caused by the difference of 0.46 mm between the two diameters of the pipes.

When required OMS can take this process as step further and create a SCR (HiLo < 0.5 mm) quality fit up for large UOE pipes by additionally sorting the pipes into sizes and shapes that will match together almost perfectly consider the pipe shape variations. Complete critical SCR pipes or fatigue sensitive pipes have been laid using this method with Hi/Lo's achieved of 0.5mm or less.

E.G. Shell Amberjack, Technip PDET and Simian Sapphire

Example 4. Avoiding pipe geometry problems by counterboring

The ultimate method of solving pipe geometric problems, which by now the reader will have gained an understanding are both common and expensive, is to take the step of attempting to create a perfectly round pipe. This is typically achieved by counterboring the pipes to a specific size. You would imagine that this would be an easy process, however reality is that pipes not only vary in shape but also in size. As a consequence, counterboring to one size might mean that considerable sections of some pipes would be missed and not be counterbored at all whilst in other pipes it might mean that the wall thickness was reduced too much (resulting in the pipe being out of specification). Neither situation is acceptable. What OMS provides is the measurement and analysis solution that removes minimal wall thickness (by producing counterbore groupings) so that no partial counterbore or wall thickness problems occur. Our extensive experience of undertaking this type of work has resulted in a system that has been proven to give maximum utilisation of the pipe material for each pipe.



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This figure give an indication of the material that would be removed from a pipe during counterboring. The amount of material varies from a little more than 0.5 mm in one location on the pipe to as much as 3 mm in one area. The resulting wall thickness of the pipe varies by less than 0.8 mm after the machining process has been completed. OMS tools can be used to measure the pipe shape before counterboring in order to determine the right counterbore group size and then to measure the pipes after counterboring in order to ensure that the counterbore tool performed correctly.

E.G. Chevron/Subsea7/Petrology Blind Faith and Shell/Subsea7/Petrology BC10

Conclusion

OMS specialise in providing value added solutions to the pipe laying process. We additionally supply tools to measure a wide variety of dimensional features on pipes. For more information regarding our pipe measurement technology and/or if you would like a discussion regarding any fit-up issues please contact:

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